

BEAM THEORY – STRESS ANALYSIS

STRUCTURAL MECHANICS

The ERAMCA Project

Environmental Risk Assessment and Mitigation on Cultural Heritage assets in Central Asia

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LECTURER/STUDENTS OBJECTIVES

-  Describe the internal forces exerted by neighbouring particles and present the fundamental concept of stress for beams.
-  Understand the equilibrium of beams by means of internal surface forces (stress).

INTRODUCTION

STRESS DEFINITION

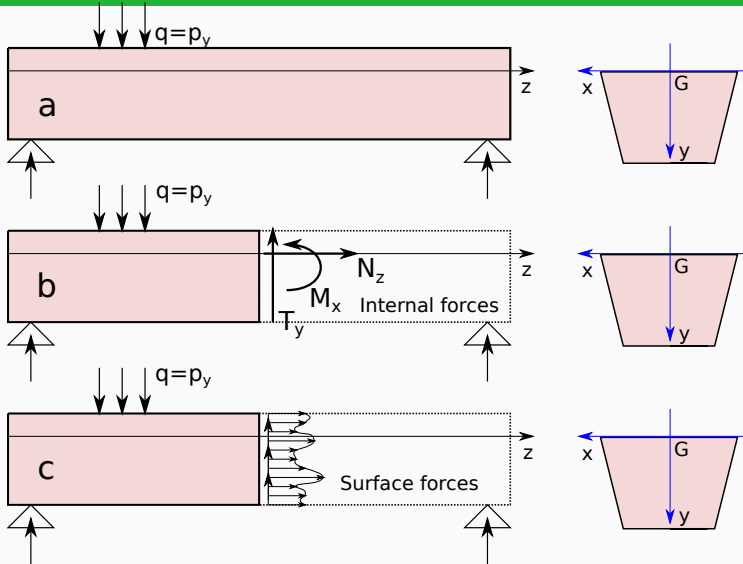
The mathematical description of equilibrium conditions lead to the idea of **stress**.

- The concept of **stress** is fundamental for the study of **continuum mechanics**
- The first contributions are by **A.L. Cauchy** who formulated a theory in 1822, based on the idea of **pressure** in fluids



A beam or a structure must be:

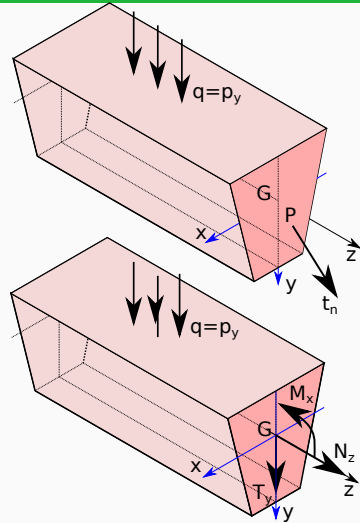
- a **globally** in equilibrium: the external loads and the reactions from support must be a system of forces in equilibrium
- b in equilibrium for every possible part: the external loads and the **internal forces** N_z , T_y and M_x (that represent **global** forces on the section of the cut) must be a system of forces in equilibrium
- c in equilibrium for every possible part: the external loads and the **stresses** (surface forces acting on every **point** on the section of the cut) must be a system of forces in equilibrium



EQUILIBRIUM OF A PORTION OF THE BEAM: STRESS

Surface forces called **stresses** (\mathbf{t}_n) must be present on the cut face to reach **equilibrium**

The resultant of these surface forces must be **equivalent** to the internal forces

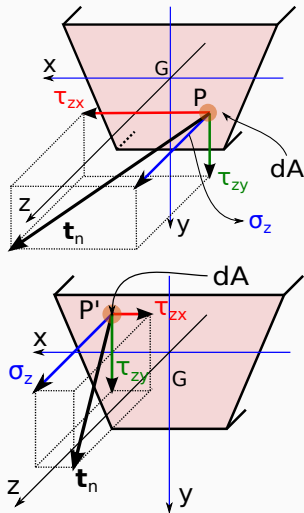


STRESS COMPONENTS

The components of the stress vector \mathbf{t}_n acting on a point P of the cross section of the beam are **three**: τ_{zx} , τ_{zy} (shear or tangential stress) and $\sigma_{zz} = \sigma_z$ (normal stress)

The first subscript refers to the z axis **orthogonal** to the cross section, the second the **direction** of the stress

For other points (P') of the same cross section, vector \mathbf{t}_n may have different **magnitude** and **direction**, i.e., $\mathbf{t}_n = \mathbf{t}_n(P) = \mathbf{t}_n(x, y)$



WHAT DO INTERNAL FORCES REPRESENT?

The internal forces are the **resultant** of the...

... stress vector \mathbf{t}_n components σ_z , τ_{zx} and τ_{zy}

$$N_z = \int_A \sigma_z \, dA$$

$$M_x = \int_A \sigma_z y \, dA$$

$$M_y = - \int_A \sigma_z x \, dA$$

$$T_x = \int_A \tau_{zx} \, dA$$

$$T_y = \int_A \tau_{zy} \, dA$$

$$M_z = \int_A (\tau_{zy} x - \tau_{zx} y) \, dA$$

For a plane structure (or for symmetrical forces) the internal forces are **three** (i.e., N_z , T_y , M_x), otherwise they are **six**

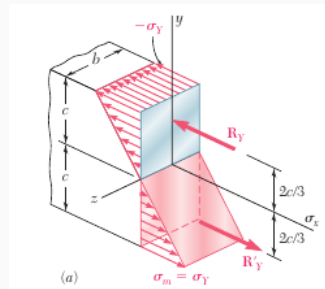
Note that integration (\int_A) is a **continuous sum**; summation ($\sum_{i=1}^N$) is a **discrete sum**!

HOW TO FIND STRESSES?

If the beam is **statically determinate**, N_z , T_y e M_x are found by using **equilibrium equation** only; if the beam is **statically indeterminate** by using **compatibility equations**

To find the stresses from the previous equations...

... their **distribution** over the area A of the cross section has to be known (wait next lectures!)



SIGN CONVENTIONS FOR STRESS

- Positive stress on positive faces (z axis **pointing out**) if in the positive direction of axes
- Negative stress on negative faces (z axis **pointing in**) if in the negative direction of axes

A (principal) reference system exists where...

... the stresses are described by σ_1 , σ_2 e σ_3 only. The faces where these stresses act, the tangential stresses are zero

One principal stress is always zero for beams

Graphical procedure to find principal stresses and principal directions: Mohr's circles

RECIPROCITY OF TANGENTIAL STRESS

- Equilibrium along z axis:

$$\sigma_z(dy t) - \tau_{yz}(dz t) + \tau_{yz}(dz t) +$$

$$-\sigma_z(dy t) = 0 \quad \text{OK!}$$

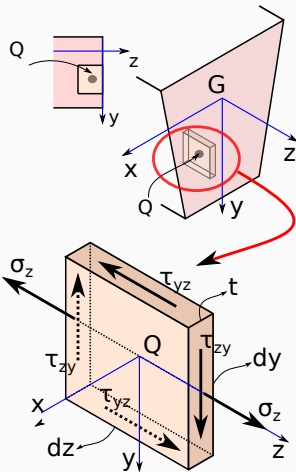
- Equilibrium along y axis:

$$-\tau_{zy}(dy t) + \tau_{zy}(dy t) = 0 \quad \text{OK!}$$

- Equilibrium about x axis:

$$\tau_{yz}(dz t) \left(\frac{dy}{2} \right) + \tau_{yz}(dz t) \left(\frac{dy}{2} \right)$$

$$-\tau_{zy}(dy t) \left(\frac{dz}{2} \right) - \tau_{zy}(dy t) \left(\frac{dz}{2} \right) = 0 \quad \text{i.e.,} \quad \tau_{zy} = \tau_{yz}$$



| Parameter | Physical dimensions | SI unit |
|--|---------------------|---------|
| Stress $\sigma_z, \tau_{zx}, \tau_{zy}$ | FL^{-2} | Pa |
| Area $A, d\Omega_x, d\Omega_y, \dots, d\Omega_z$ | L^2 | m^2 |
| q, p_y | FL^{-1} | N/m |